

Sicherheit in Technik und Chemie

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#### PRESENTATION OF INTERDISCPLINARY PROCECT ON HEA PROCESSING

# SURDIA (SURFACE DEGRADATION PHENOMENA AND UTILIZATION OF INNOVATIVE ALLOYS) - CURRENT R&D AT BAM -

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# HEAs on the way for application in components



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# Interdisciplinary collaboration to investigate degradation by processing





08.10.2021 Processing of HEAs/MEAs and influence on application properties - R&D at BAM Berlin

### **Current research at BAM Berlin**



nthesis laboratory

ng facility

naces

#### Basic research on HEAs/MEAs:

- Weldability by
  - Tungsten Inert Gas (TIG) Welding and
  - Friction Stir Welding (FSW)
- Machinability by
  - Conventional milling and
  - Ultrasonic assisted milling

#### Processing influence on application properties

- Mechanical performance of welded joints
- Surface integrity  $\rightarrow$  electrochem. and high-temperature corrosion
- Hydrogen diffusion and adsorption





### Experimental -Materials



At%	Со	Cr	Fe	Mn	Ni	HV 0.5
HEA	19.7	20.7	19.6	20.1	19.9	172
MEA	33.0	34.3	-	-	32.7	251

Preparation of two alloys (provided by group of Jun.-Prof. G. Laplanche, RUB):

- 1. Vacuum induction melting of elements (99.9 wt.-% purity)
- 2. Homogenizing (1200 °C for 48 h)
- 3. Rotary swaging (from diameter 40 mm to 16 mm)
- 4. Recrystallization (HEA: 1020 °C, MEA: 1060 °C, for 1 h)







 Weldability is a subject to a complex interaction of material, welding process conditions and construction/component design

#### → Current research regarding HEAs focusses on material and welding process interactions

## Welding of HEAs Typical welding defects

#### Welding process related defects

- Pores
- Tunnel defects
- Slag inclusions...
- $\rightarrow$  Process parameter adaption

#### Material related welding defects

Hot cracking (T > 200°C)

 Solidification cracks, liquation cracks

Cold cracking (T <  $200^{\circ}$ C)

- Hydrogen assisted cracking, Hardening cracks (phase transformation)
- → Temperature control (e.g. preheating, post weld heat treatment-PWHT)





### Welding of HEAs First time bead-on-plate TIG welding



Shielding gas



Sample (14x80 mm)

- Shielding gas : Argon
- Root shielding gas: Argon + 7,5 % H<sub>2</sub>

## Welding of HEAs Bead-on-plate TIG welding of CoCrFeMnNi-HEA

![](_page_8_Picture_1.jpeg)

#### Top side

![](_page_8_Picture_3.jpeg)

- Full penetration
- Heat tint colors in weld seam vicinity ( $\rightarrow$  corrosion resistance!)
- Pores in weld metal ( $\rightarrow$  fatigue behavior?)
- Risse in der WEZ ( $\rightarrow$  general defect-free welding possible?)

## Welding of HEAs Bead-on-plate TIG welding of CoCrFeMnNi-HEA - Microstructure

![](_page_9_Picture_1.jpeg)

- Dendritic microstructure of weld metal  $\rightarrow$  micro-segregations
- Intergranular cracks in heat-affected zone (HAZ) of base material

![](_page_9_Figure_4.jpeg)

## Welding of HEAs Bead-on-plate TIG welding of CoCrNi-MEA

![](_page_10_Picture_1.jpeg)

![](_page_10_Picture_2.jpeg)

![](_page_10_Picture_3.jpeg)

- Full penetration
- Heat tint colors in weld seam vicinity ( $\rightarrow$  corrosion resistance!)
- Pores in weld metal ( $\rightarrow$  fatigue behavior?)
- Risse in der WEZ (→ general defect-free welding possible?)

### Welding of HEAs Bead-on-plate TIG welding of CoCrNi-MEA - Microstructure

![](_page_11_Picture_1.jpeg)

- Dendritic microstructure in weld metal

- Also intergranular cracking in HAZ

![](_page_11_Picture_4.jpeg)

### Welding of HEAs Could solid state welding be the answer instead of fusion welding?

![](_page_12_Picture_1.jpeg)

Recently, pre-studies at BAM for process development:

![](_page_12_Figure_3.jpeg)

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## Welding of HEAs Friction stir welding – challening parameter adaption (ongoing work)

![](_page_13_Picture_1.jpeg)

### Machinability and surface integrity

![](_page_14_Picture_1.jpeg)

 Machinability characterized by: cutting force, tool wear & life, chip formation and surface integrity

![](_page_14_Figure_3.jpeg)

 → Surface integrity is the key challenge for machinability of components in highly stressed or safety-relevant areas

#### Machinability and surface integrity Parameters for milling tests

![](_page_15_Picture_1.jpeg)

![](_page_15_Figure_2.jpeg)

cutting speed feed rate per cutting edge

- rotational speed
- feed rate
- cutting depth
  - feed force in

feed-/ x-direction

passive force in depth-/ z-direction

## Machinability and surface integrity Regarded parameters for milling tests

![](_page_16_Picture_1.jpeg)

![](_page_16_Picture_2.jpeg)

![](_page_16_Picture_3.jpeg)

- 6 mm ball nose end milling tool with 4 cutting edges (cemented carbide / PVD coated)
- Ultrasonic assisted milling (USAM modified 5-axis machining portal)
- 3D-cutting force analysis with a dynamometer (Kistler)

## Machinability and surface integrity Tool wear - Comparison HEA and MEA

![](_page_17_Picture_1.jpeg)

Unused cutting edge (as delivered)

![](_page_17_Picture_3.jpeg)

![](_page_17_Figure_4.jpeg)

Used cutting edge HEA-tests

![](_page_17_Picture_6.jpeg)

Used cutting edge MEA-tests

![](_page_17_Picture_8.jpeg)

- Cutting edges almost "as good as new" after machining experiments at HEA specimens
- → Very low tool wear with HEA (CoCrFeMnNi)
- Severe wear marks and breaks at the tool tip after machining experiments at MEA specimens
- → Applied cutting tool not suitable for MEA (CoCrNi)

## Machinability and surface integrity Topography/Defects - CoCrNi-Alloy

![](_page_18_Picture_1.jpeg)

![](_page_18_Figure_2.jpeg)

- First tests: high surface quality, almost free of defects
- Significant influence of tool wear on the generated surface

#### → Worn tool causes extensive surface defects (break-outs)

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# Machinability and surface integrity Residual Stresses (XRD) - Comparison HEA and MEA

#### CoCrFeMnNi-HEA

#### **CoCrNi-MEA**

![](_page_19_Figure_3.jpeg)

 USAM causes reduced detrimental tensile residual stresses below the surface in the CoCrFeMnNi-HEA compared to conventional milling

#### $\rightarrow$ Improved residual stress condition due to application of USAM

 With the CoCrNi-MEA the continuously increasing tool wear has a predominant influence on the residual stress state

### **Summary and conclusions**

![](_page_20_Picture_1.jpeg)

#### Basic research on HEAs/MEAs:

- Weldability/Machinability:
  - ➤ TIG fusion welding results in cracking of HAZ, Solid-state FSW promising technique → general weldability is ongoing work
  - ➤ Cracks perhaps originate from Cu-slags from EDM-cutting → in-depth characterization of different weld zones and properties necessary
  - Ultrasonic assisted milling for improved surface integrity and reduced reaction forces

#### Processing influence on application properties

- Mechanical performance of welded joints still open
- Surface integrity → electrochem. and high-temperature corrosion experiments are in progress
- Hydrogen diffusion and adsorption experiments in progress

#### **Further topcis: Electrochemical corrosion properties**

- Micro-segregations of elements during laser welding
- Investigated with scanning kelvin probe force microscopy
- Visualization of local Volta-potential

![](_page_21_Figure_5.jpeg)

- Epitaxial growth of dendrites from fusion line during solidification
- $\rightarrow$  Segregations of elements  $\rightarrow$  increased pitting susceptibility
- Dissolution and reprecipitation of Al-rich impurities (due to processing)
- $\rightarrow$  Smaller difference potential  $\rightarrow$  galvanic corrosion risk decreases in WM

![](_page_21_Picture_10.jpeg)

### Further topics: Hydrogen diffusion in HEAs/MEAs

![](_page_22_Picture_1.jpeg)

#### CoCrFeMnNi-HEA

#### - CoCrNi-MEA

![](_page_22_Figure_4.jpeg)

- Similar diffusion behavior, i.e. active traps at respective temperatures
- CoCrFeMnNi: significantly higher hydrogen concentration (higher effusion rate!)
- $\rightarrow$  Concern for hydrogen assisted (weld) cracking

# Thank you for your kind attention!

![](_page_23_Picture_1.jpeg)

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