



Strengthening mechanisms of single crystalline CrCoNi and CrMnFeCoNi at creep temperatures above 700°C

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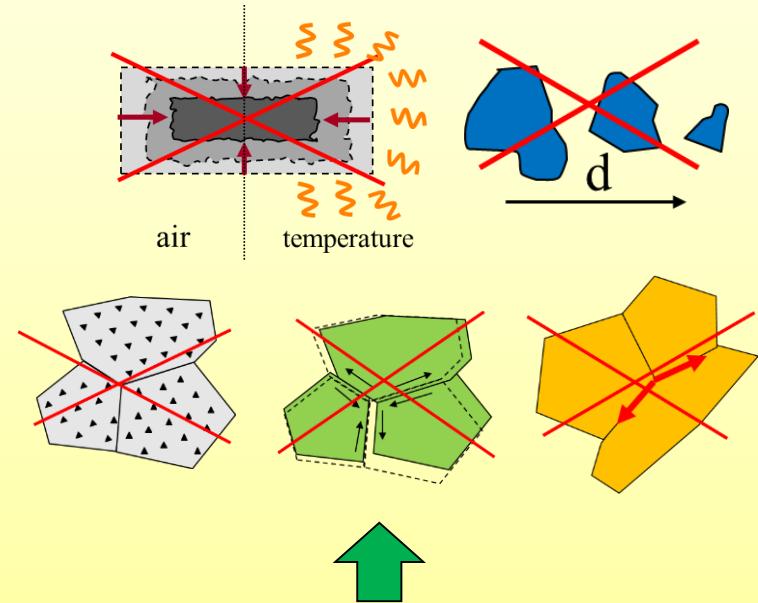


Motivation

Investigation of temperature dependent solid solution strengthening in single phase multicomponent alloys with medium and high entropy using creep testing

Possible negative effects:

- Oxidation effects during experiments in air and different temperatures
- Grain size effects
- Sliding processes at the grain boundaries
- Diffusion processes at the grain boundaries
- Effects occurring due to precipitation



Realization / Solution :

- Creep testing under high vacuum ($2 \cdot 10^{-4}$ Pa)
- Using single-phase multi-component alloys: **medium and high entropy alloy (MEA + HEA)**
- Use of single crystalline materials: **investigated alloys and reference**



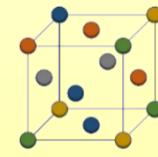
Material selection

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
1a	IIa	IIIb	IVb	Vb	VIb	VIIb	VIIIb		lb	IIb	IIIa	IVa	Va	Vla	VIIa	VIIa	
H																	He
Li	Be																
Na	Mg																
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Rb	Sr	Y	Zr	Nb	Mn	Tc	Pt	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Cs	Ba	La	Hf	Ta	V	Re	Os	Ir		Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	Ac	Rf	Ha	S	Ns											

Periodic tabel of elements:
<http://www.chemgapedia.de>

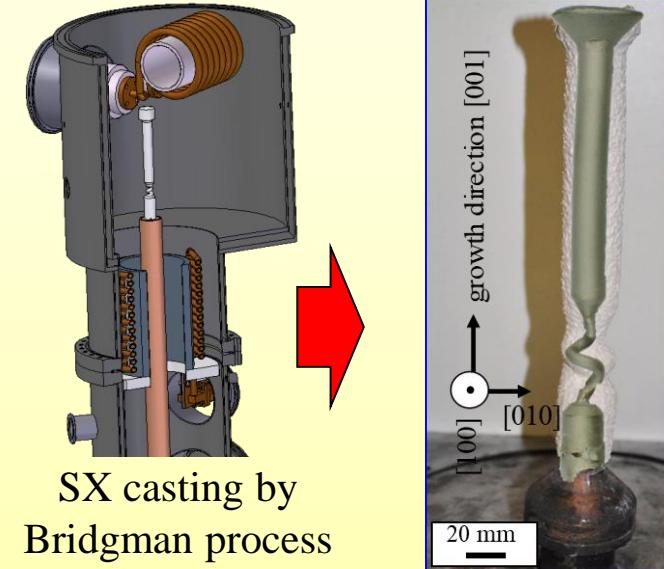
MEA
 $\text{Cr}_{33,3}\text{Co}_{33,3}\text{Ni}_{33,3}$ (in at.%)
 fcc solid solution
 $S_{\text{conf}} = 1,1 \cdot R$ in $\text{J}/(\text{mol} \cdot \text{K})$

HEA
 $\text{Cr}_{20}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{20}$ (in at.%)
 Cantor Alloy
 fcc solid solution
 $S_{\text{conf}} = 1,6 \cdot R$ in $\text{J}/(\text{mol} \cdot \text{K})$

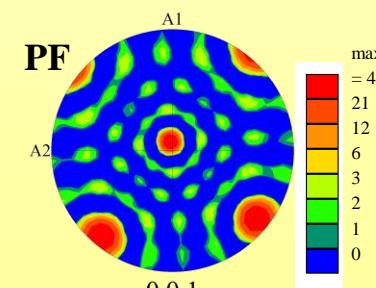


similar atomic radius

Reference material:
 fcc pure Nickel
 $S_{\text{conf}} = 0 \cdot R$ in $\text{J}/(\text{mol} \cdot \text{K})$



SX casting by
Bridgman process



EBSD
Quality check

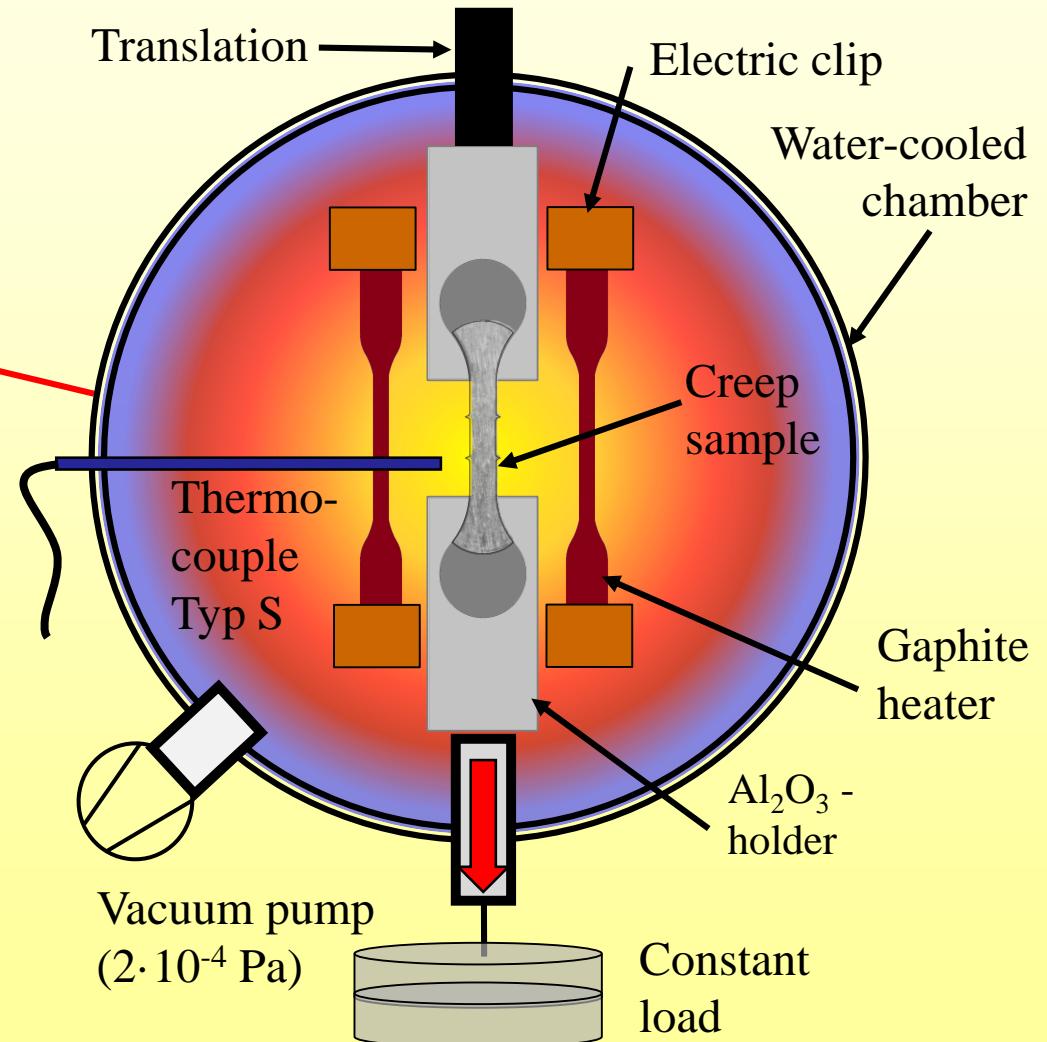
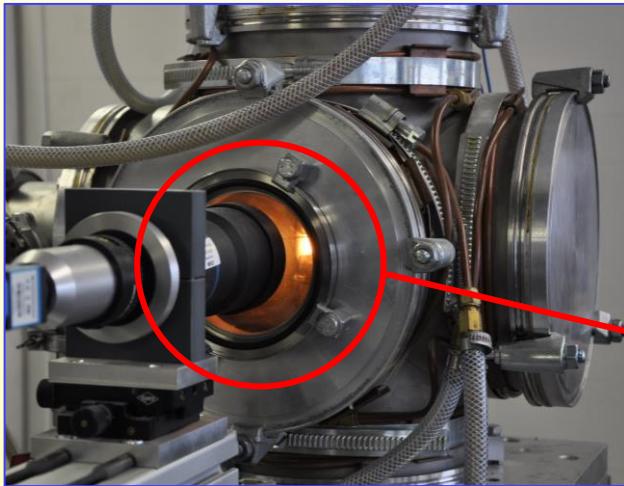


Wire EDM
Sample preparation



Mechanical testing

Creep testing under vacuum

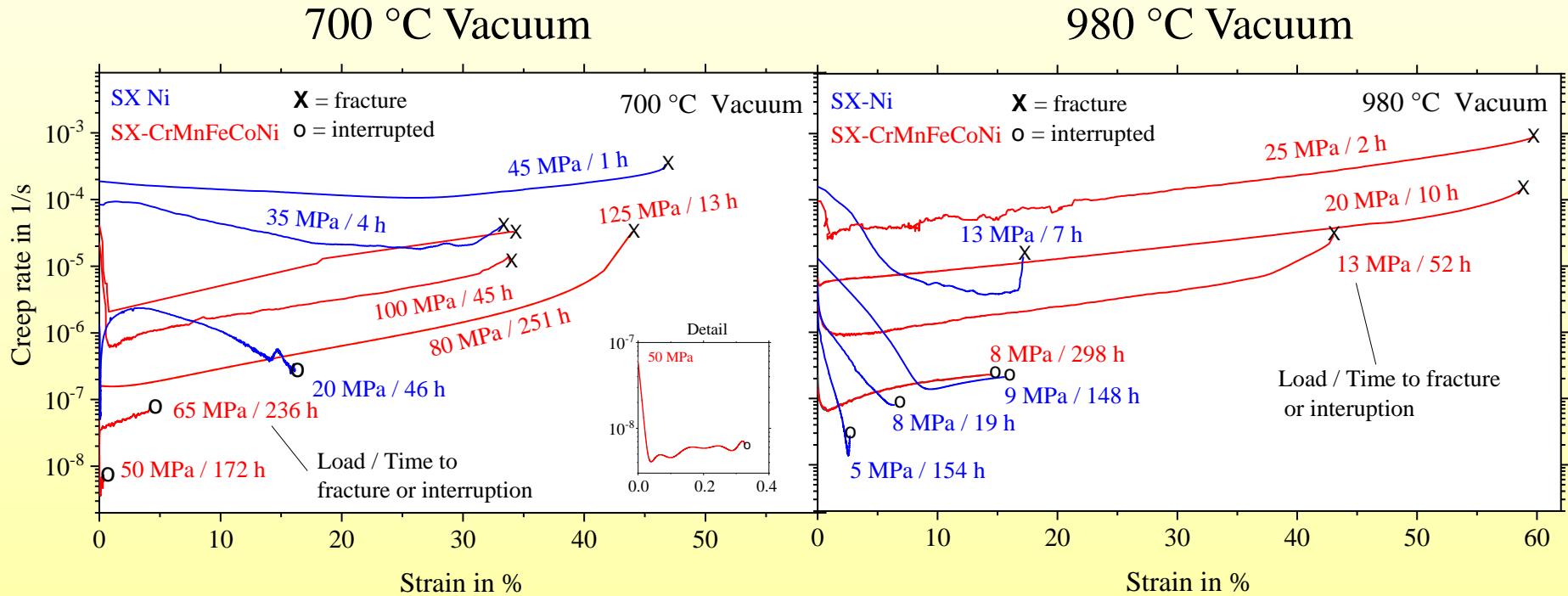


Testing conditions

Atmosphere: vacuum $2 \cdot 10^{-4}$ Pa
Temperatures: 700 / 980 / 1050
1100 and 1200 °C
Constant Load: 2 to 125 MPa
Geometry: 27x2.9x1 mm³



Comparison 700 and 980 °C SX-CrMnFeCoNi and SX-Ni

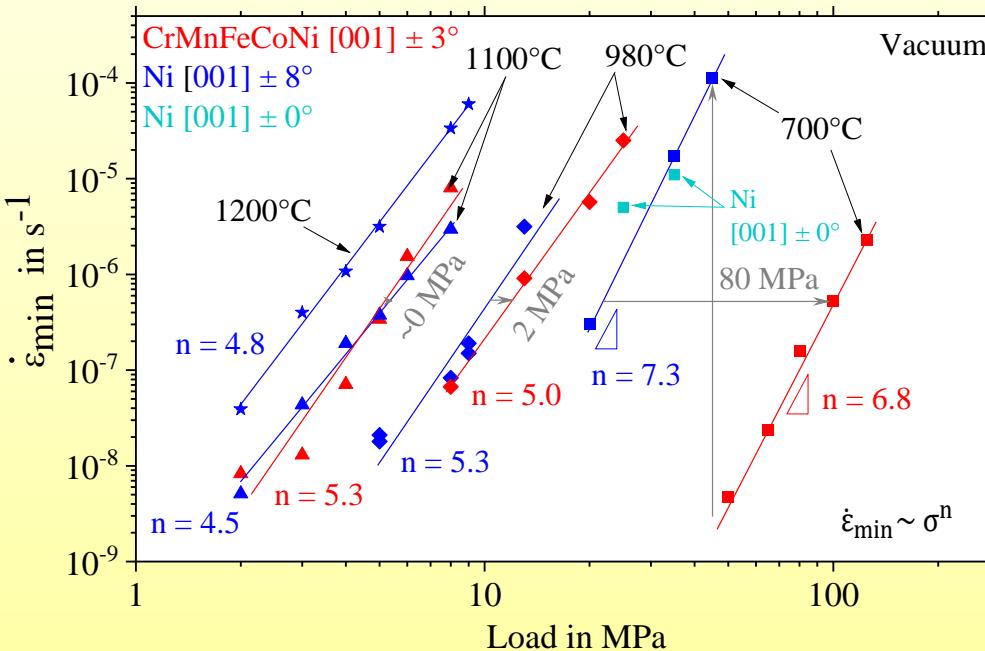


- Test carried out from 700 to 1200 °C and interrupted in some cases for TEM-investigations

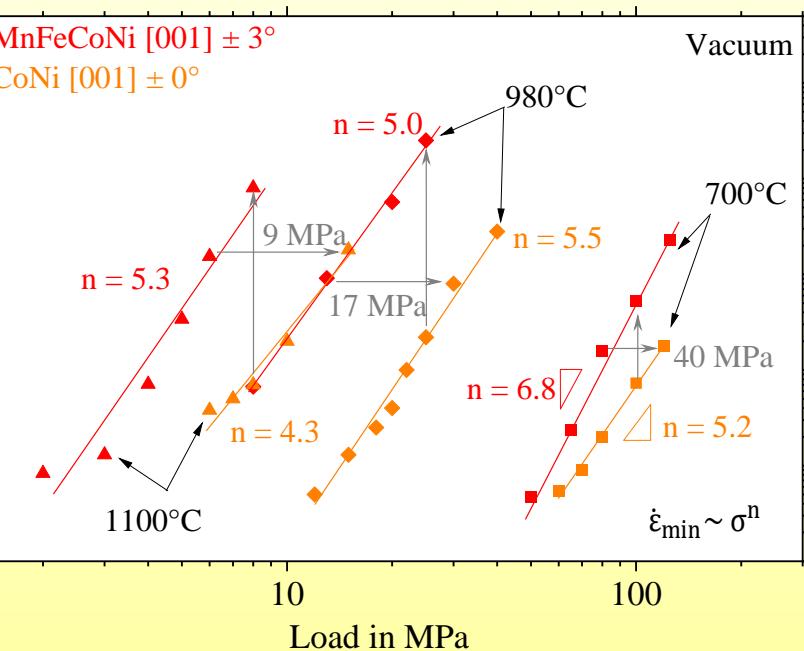


Norton Plot 700 – 1200°C

Ni and CrMnFeCoNi



CrCoNi and CrMnFeCoNi



- Decreasing stress difference from 80 MPa to 0 MPa from 700 to 1100 °C

Solid solution strengthening at lower temperatures of 700 °C

- Decreasing stress difference from 40 MPa to 9 MPa from 700 to 1100 °C

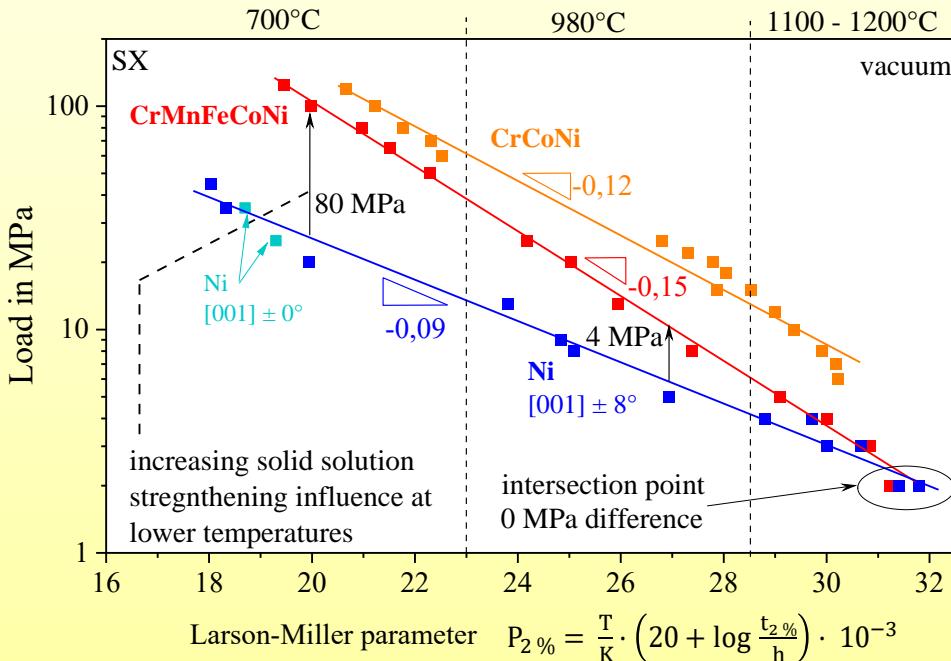
Further strengthening mechanisms could be active in the CrCoNi alloy



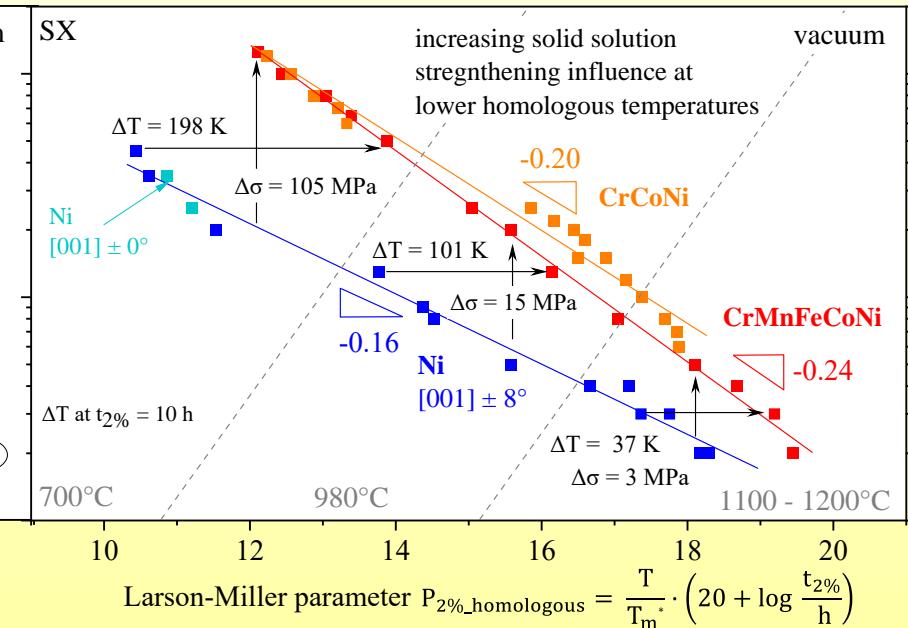
Larson-Miller Plot

700 – 1200°C

Absolut temperature



Homologous temperature



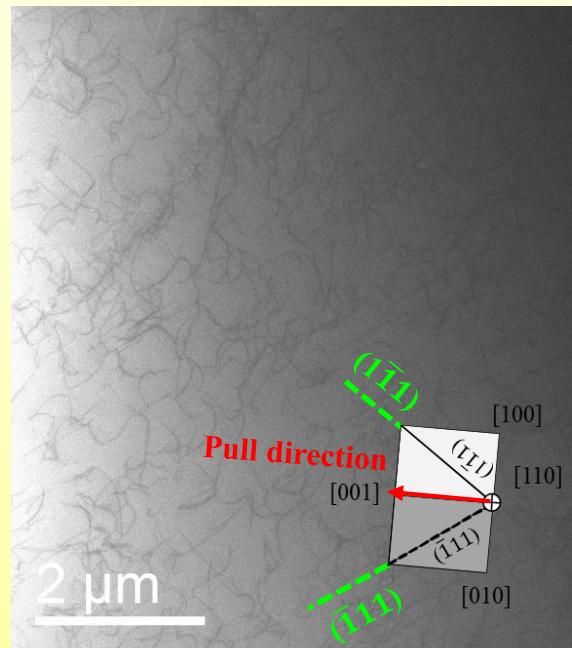
- Flatter slope of -0.09 for pure nickel in comparison to CrCoNi and CrMnFeCoNi with -0.12 and -0.15
- Comparable behavior of CrCoNi and CrMnFeCoNi in relation to homologous temperature

Solid solution strengthening recognisable

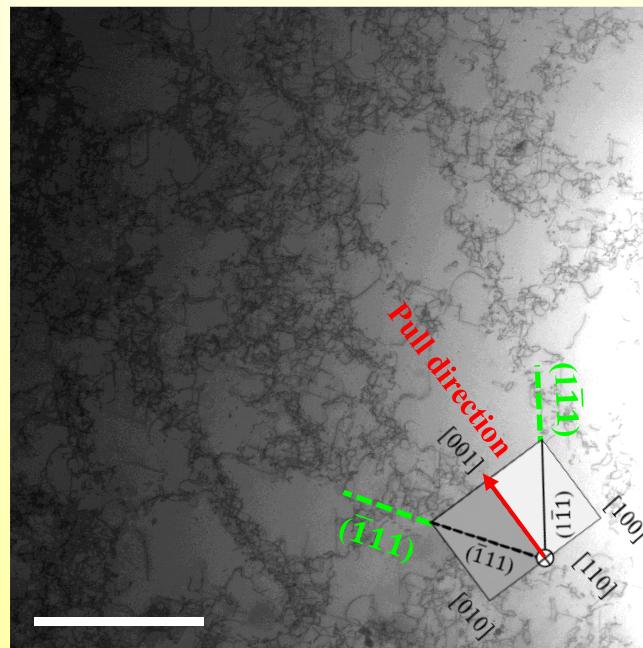


Interrupted creep tests at 700°C Ni, CrCoNi and CrMnFeCoNi TEM-analysis

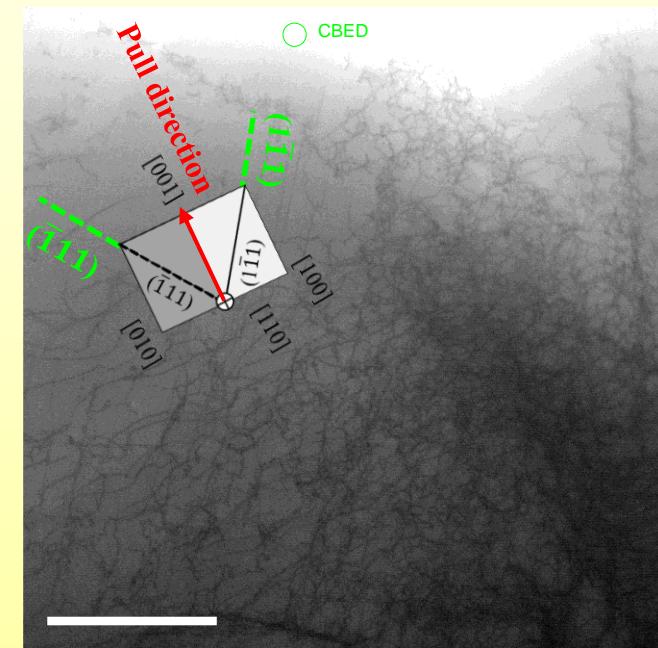
pure Ni



CrCoNi



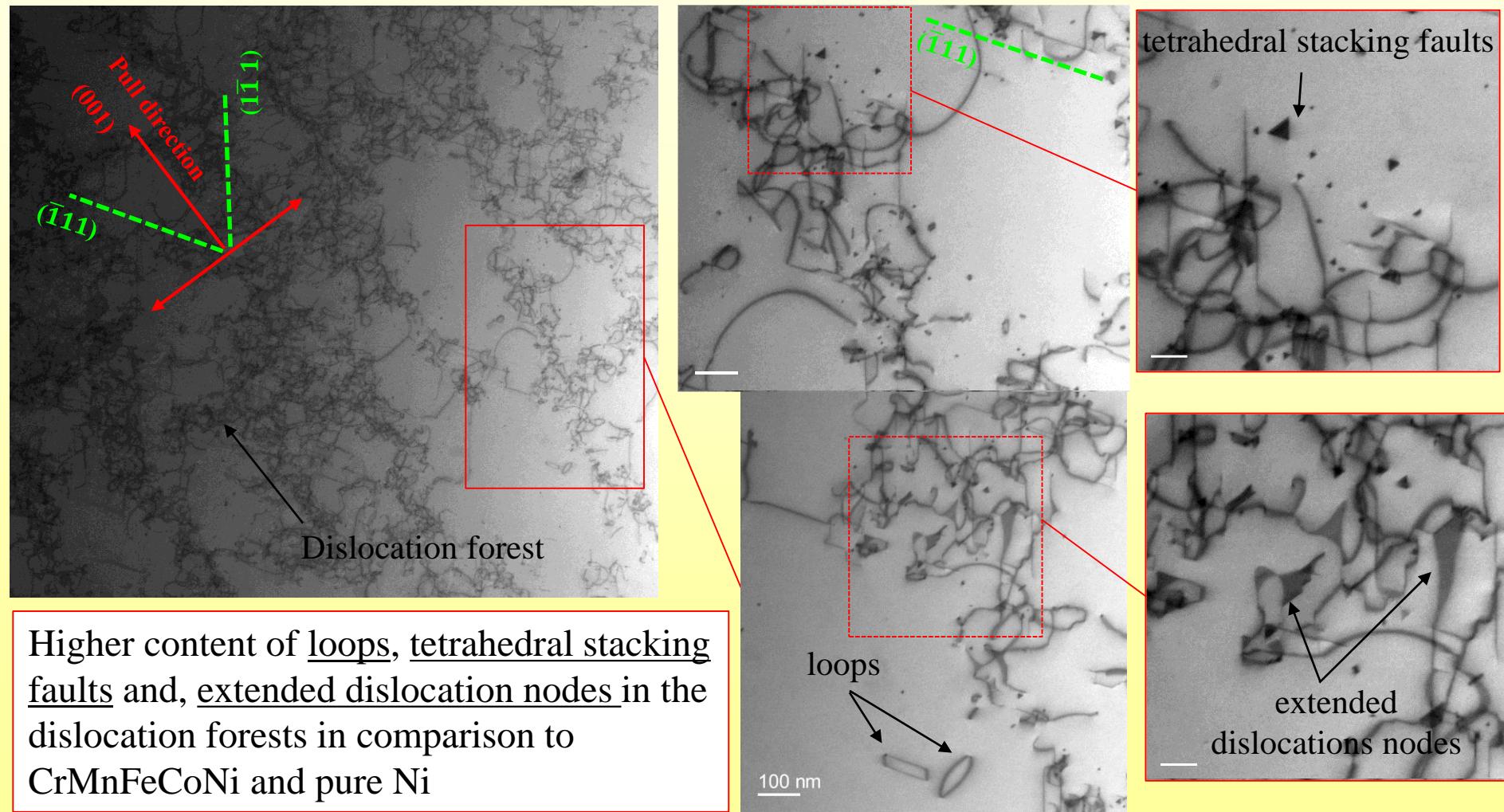
CrMnFeCoNi



- homogenous dislocation distribution
- low content of stacking faults
- inhomogeneous distribution: areas with higher dislocation content and areas with no or low dislocation content
- Dislocation networks (with high dislocation density) → dislocation forest structure



CrCoNi-SX 700 °C 120 MPa (interrupted) TEM-analysis





Summary



- The single phase alloys CrCoNi and CrMnFeCoNi were successfully cast as single crystals.
 - Creep tests carried out on single-phase SX-CrCoNi, CrMnFeCoNi and pure Ni from 700 to 1200 °C excluding oxidation, grain boundaries and multiphase effects.
-
- **The influence of solid solution strengthening of CrCoNi and CrMnFeCoNi increases by decreasing temperature (1200 to 700°C).**
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- **Dislocation forests occur in CrCoNi and CrMnFeCoNi in comparison to pure Ni.**
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- **Possible influence of stacking faults and extended dislocation nodes recognizable on the creep resistance for CrCoNi above 700°C.**



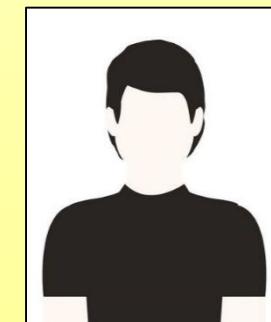
Planned work in the 2nd funding period

Material Development and Mechanical Properties of Single-Phase High Entropy Alloys



A head-and-shoulders portrait of a woman with long, straight brown hair. She is smiling warmly at the camera. She is wearing a dark green blazer over a white collared shirt.

Laura Rosenkranz



N.N.

Base alloys in the project

hcp-phase:

Y₂Gd₃Tb₂Dy₃Ho₂

*investigated in the 1st period

bcc-phase:

TiZrNbHfX

V*, Ta* and Mo

fcc-phase:

SX-CrXFeCoNi

Mn*, Pd, Ag or Au

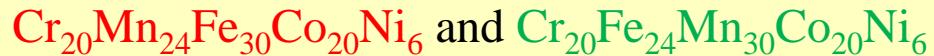


Topics in the 2nd phase

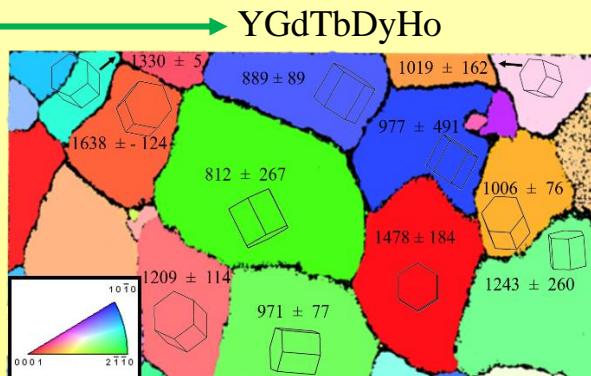
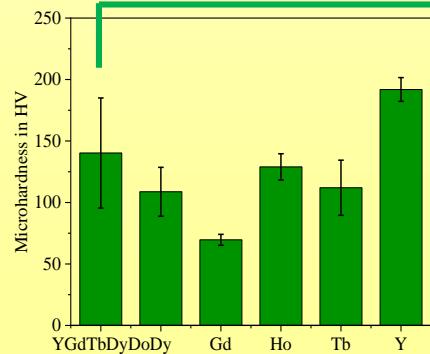
1. Intrinsic deformation process of **fcc**, **bcc** and **hcp** structured HEA

Mechanical testing: Tensile, creep and compression tests from RT to 1400 °C

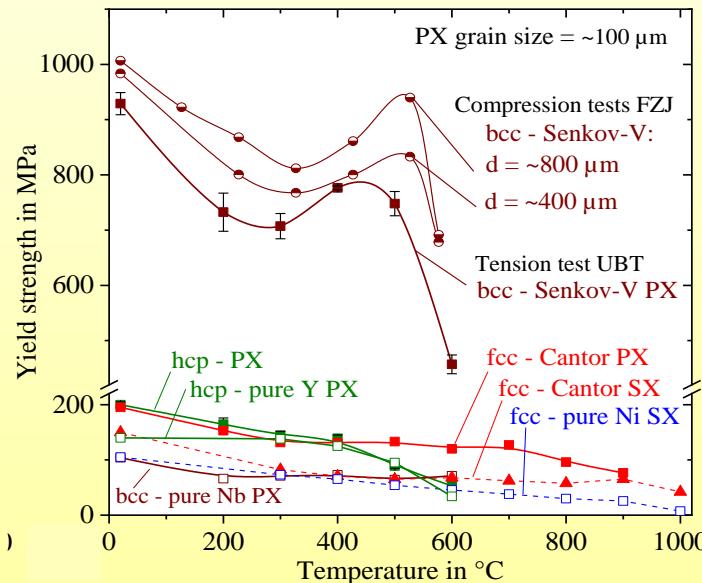
2. Stacking fault energy (using non-equiautomic **fcc**)



3. Gibbs paradox (using **hcp** HEA)



4. Yield-stress anomaly of TiZrNbHfV and further **bcc** HEA



Lienig, T., Thomas, C., Feuerbacher, M.;
Yield-stress anomaly in equiautomic
ZrNbTiVHf high-entropy alloys. ARXiv
(2019)



Thank you for your attention!

Please also read the following publication:

C. Gadelmeier, S. Haas, T. Lienig, A. Manzoni, M. Feuerbacher, U. Glatzel; **Temperature Dependent Solid Solution Strengthening in the High Entropy Alloy CrMnFeCoNi in Single Crystalline State.**
Metals 2020, 10, 1412