



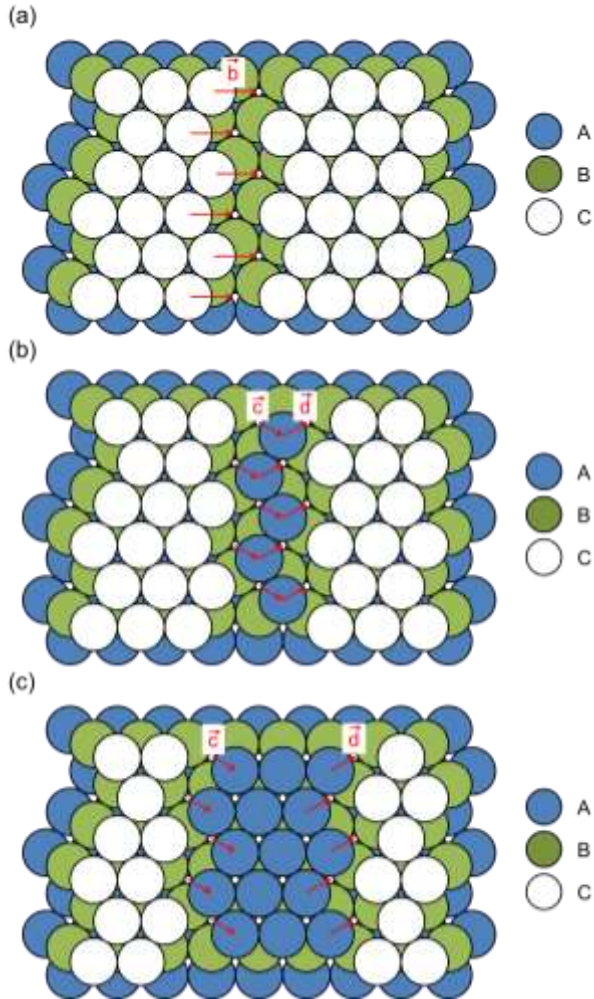
Stacking fault energy measurements in modified Cantor alloys

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Introduction



(a) Full dislocation with Burgers Vector b of type $\frac{1}{2}\langle 110 \rangle$

(b) Beginning of a dissociated dislocation (Local hexagonal stacking: ABA)

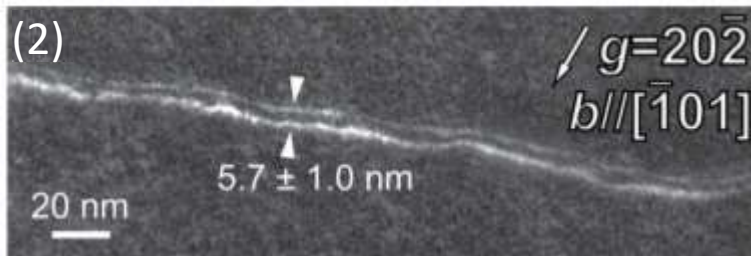
(c) Full dislocation dissociated in two Shockley partials with a stacking fault in between. Vector c and d of type $\frac{1}{6}\langle 112 \rangle$

State of the art

Stacking fault energy (SFE)

Effect of chemical composition on SFE

(1)	Alloy	Stacking fault energy (mJ/m ²)
	Cr ₁₄ Mn ₂₀ Fe ₂₀ Co ₂₀ Ni ₂₆	57.7
	Cr ₂₀ Mn ₂₀ Fe ₂₀ Co ₂₀ Ni ₂₀	25.5
	Cr ₂₆ Mn ₂₀ Fe ₂₀ Co ₂₀ Ni ₁₄	3.5



→ SFE measured:
30 mJ/m²

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(1) Zaddach et al. Mechanical Properties and Stacking Fault Energies of NiFeCrCoMn High-Entropy Alloy (2013)

(2) Okamoto et al. Size effect, critical resolved shear stress, stacking fault energy, and solid solution strengthening in the CrMnFeCoNi high-entropy alloy (2016)

Processing

As-cast ingot



Ø 45 mm

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Vacuum induction melting



500 mbar Ar

Ingot after homogenization
at 1200 °C / 48h



Ø 40 mm

Swaged from 40 down to 16.5 mm



Ø 16.5 mm

Annealing temperatures (1h) 900 °C

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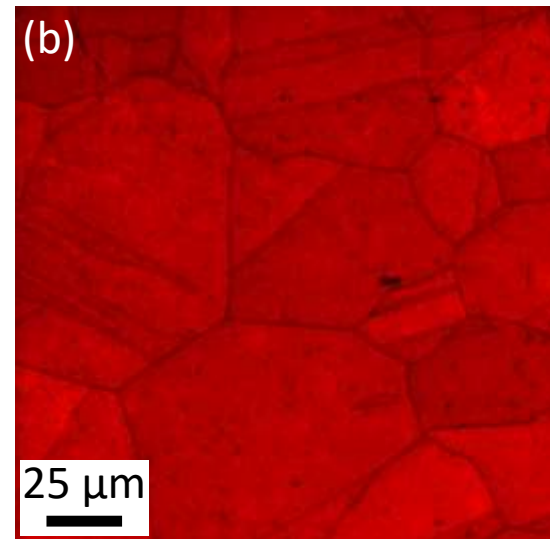
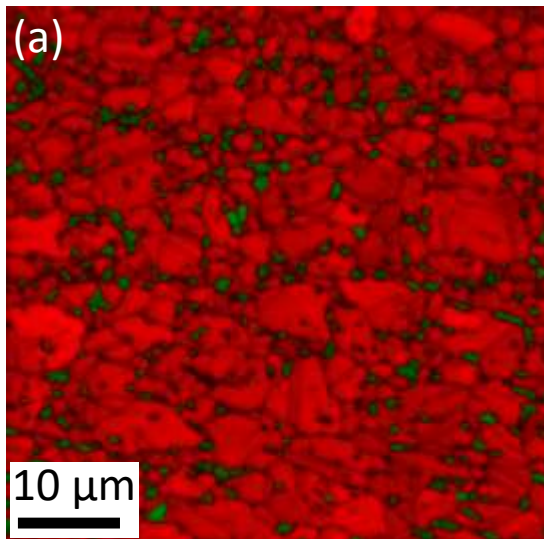
Results - Microstructure

Alloy	Heat treatment	Grain size
$\text{Cr}_{14}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{26}$	900 °C / 1h	18 μm
$\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$	1100 °C / 15 min	100 μm

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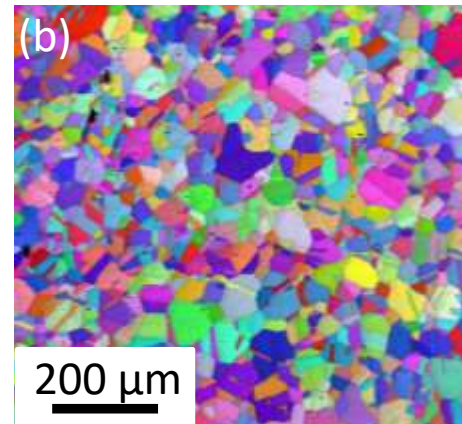
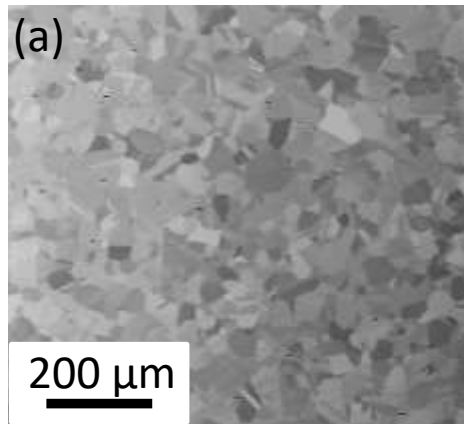


$\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$ after recrystallization (a) 900 °C for 1 h
(b) 1100 °C for 15 min

Results - Microstructure

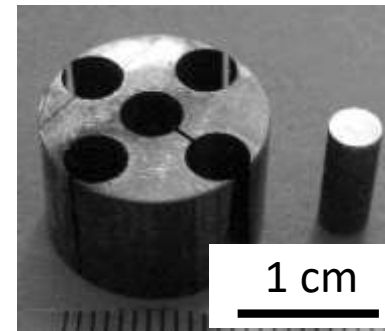
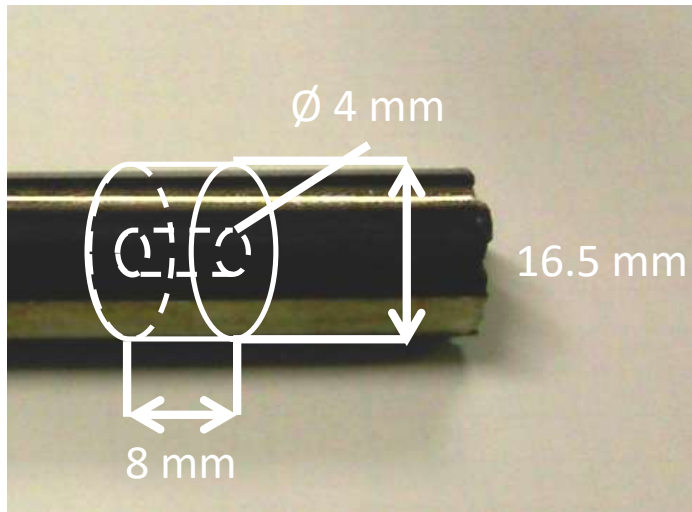
Alloy	Heat treatment	Grain size
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$\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$	1100 °C / 15 min	100 μm

- Both alloys have a single FCC solid-solution phase
- No texture was observed
- Stacking fault energy is independent of the grain size



$\text{Cr}_{14}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{26}$ after recrystallization at 900 °C for 1 h (a) BSD picture (b) EBSD mapping

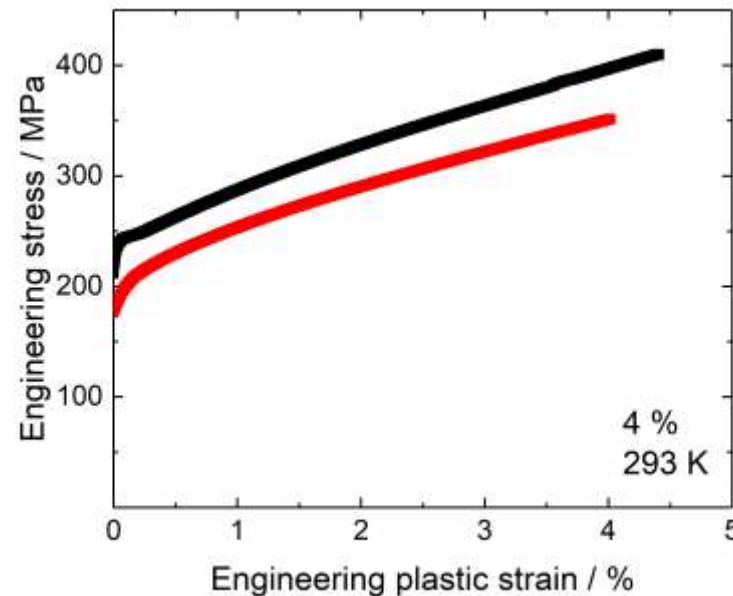
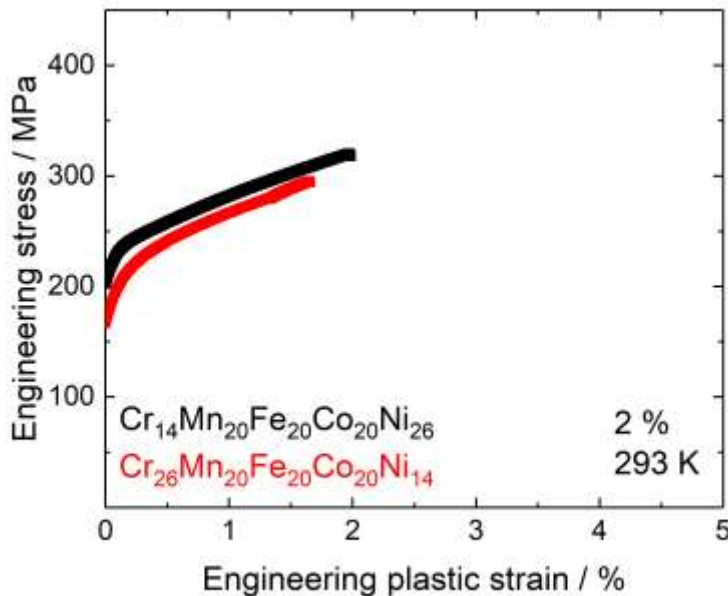
Sample preparation



Advantages:

- Many samples out of small amount of material
- Samples are easy and fast to produce

Results – compression tests



- Different yield stress $\text{Cr}_{14}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{26}$: 253 MPa
(grain size: 18 μm)
 $\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$: 216 MPa
(grain size: 100 μm)

Stacking fault energy analysis

Alloy	Stacking fault energy (mJ/m ²)
Cr ₁₄ Mn ₂₀ Fe ₂₀ Co ₂₀ Ni ₂₆	57.7
Cr ₂₀ Mn ₂₀ Fe ₂₀ Co ₂₀ Ni ₂₀	25.5
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If in Cr₁₄MnFeCoNi₂₆ SFE is 57 mJ/m²

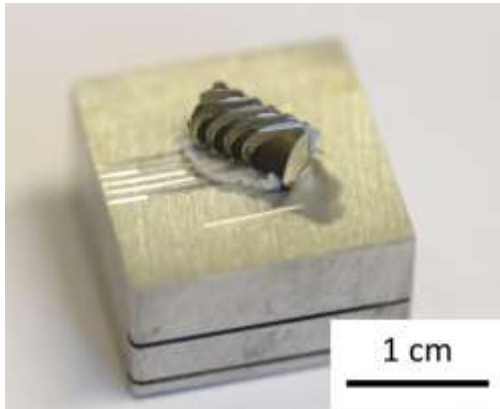
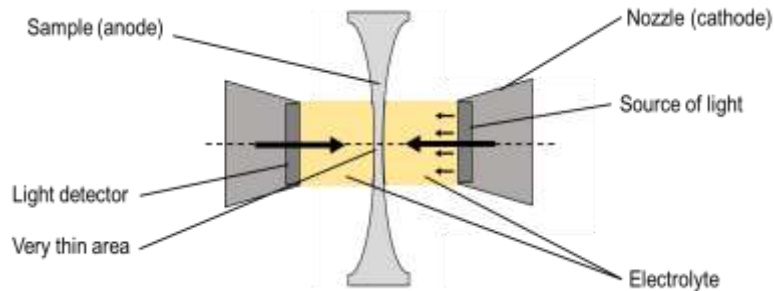
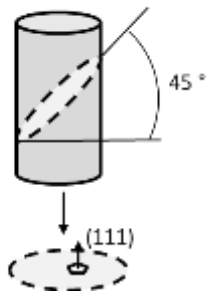
- edge dislocation spacing of 3.4 nm
- screw dislocation spacing of 1.8 nm

Stacking fault energy analysis

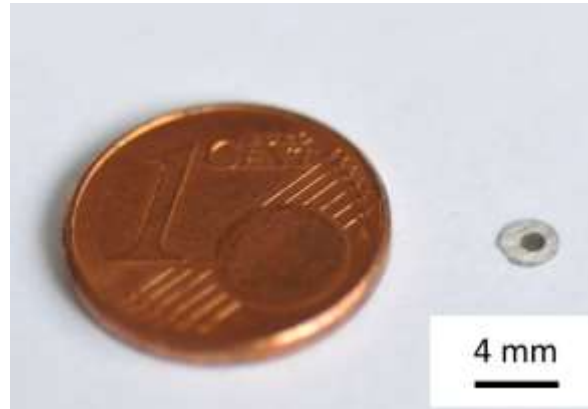
Two methods to produce TEM samples

(1) Twin jet electro polishing

Compression sample



Compression sample cut in slices



TEM sample after the electro polishing

Introduction

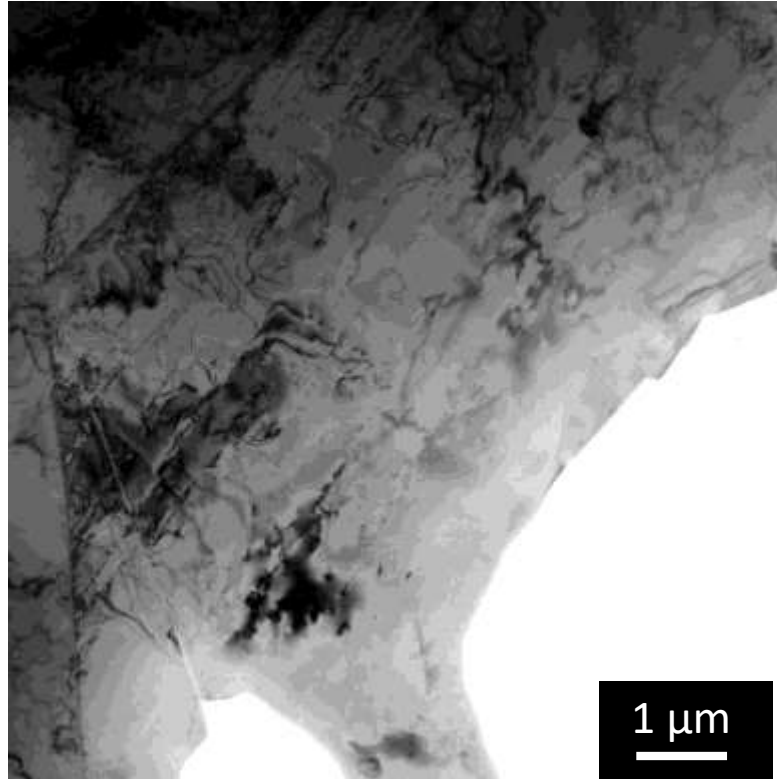
Processing

Results

Stacking fault energy analysis

Twin jet electro polishing

RUB



Bright field picture

Cr₁₄Mn₂₀Fe₂₀Co₂₀Ni₂₆ after 4 % compression

Introduction

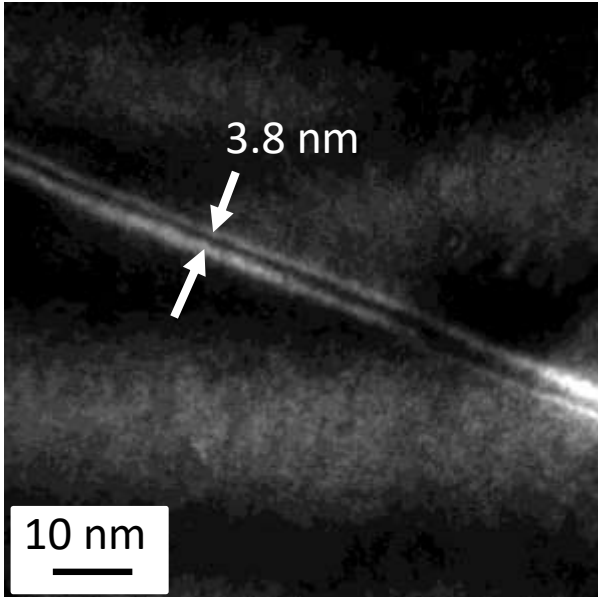
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Two methods to produce TEM samples

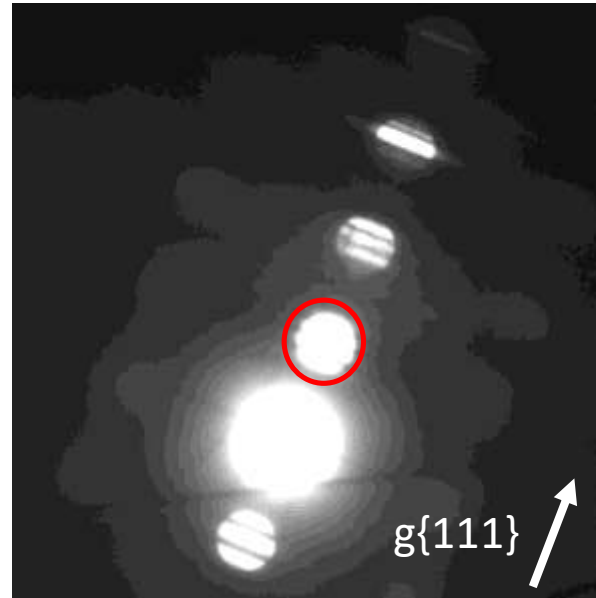
(1) Twin jet electro polishing



Weak Beam Dark Field $g/3g$

Advantages:

- Good sample quality



Diffraction

Disadvantages:

- Orientation of analyzed grains cannot be influenced

Introduction

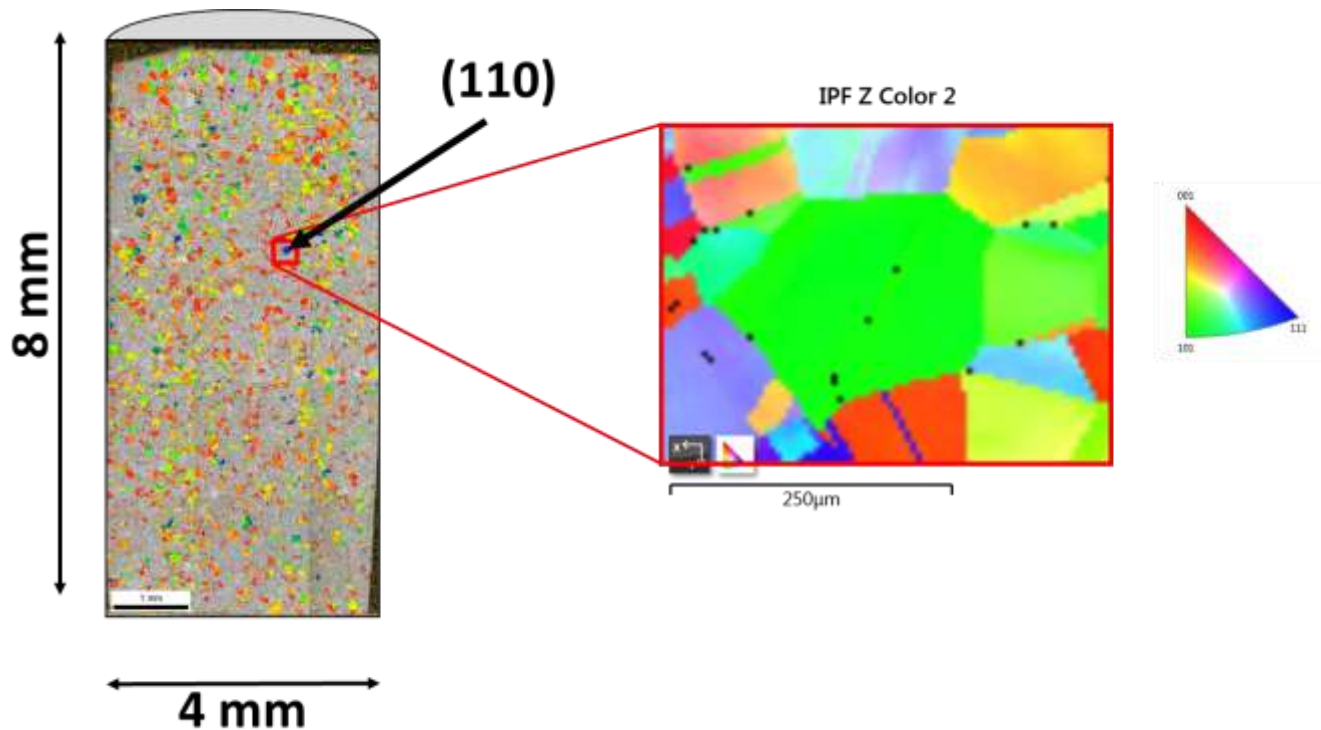
Processing

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Two methods to produce TEM samples

(1) Focused Ion Beam (FIB)



Introduction

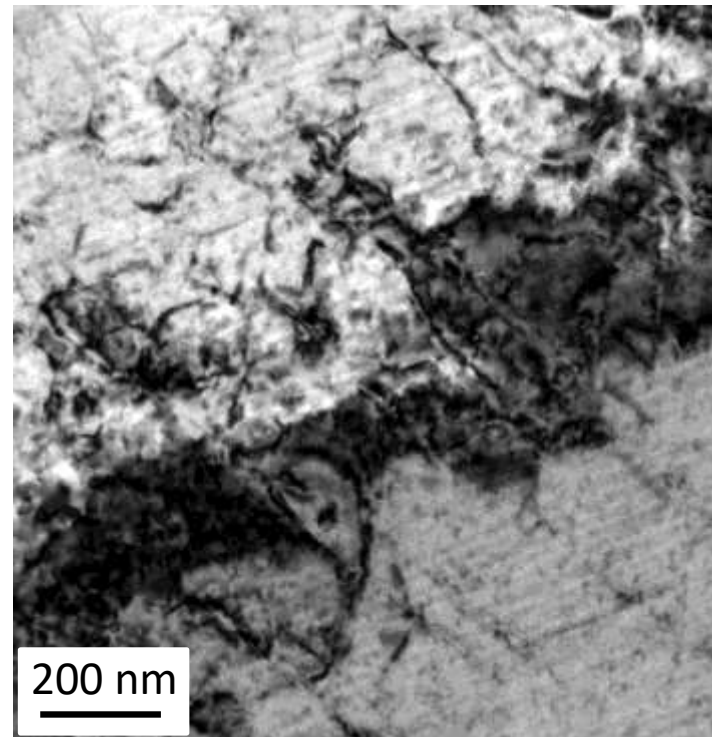
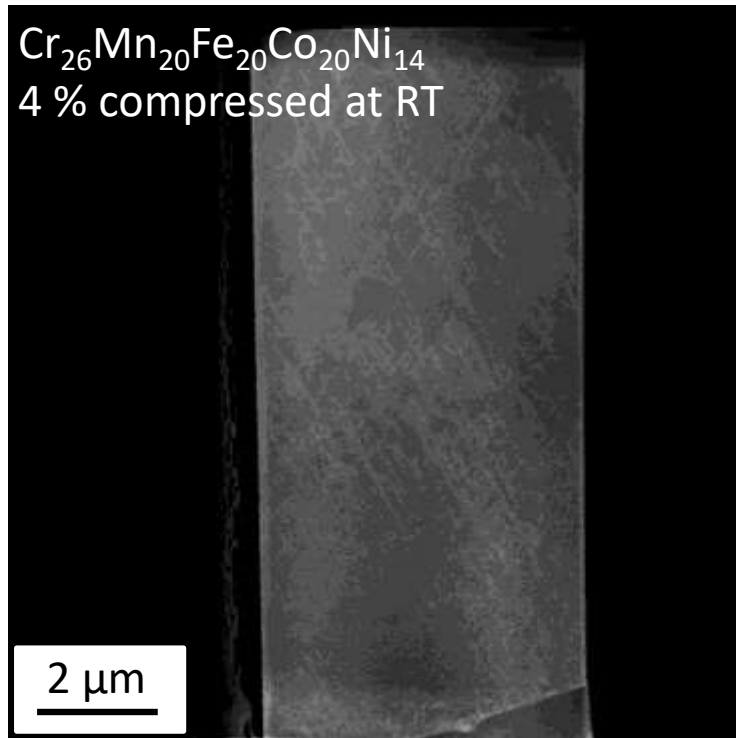
Processing

Results

Stacking fault energy analysis

Two methods to produce TEM samples

(2) Focused Ion Beam (FIB)



Advantages:

- Perfect orientation of grain

Disadvantages:

- Bad sample quality

Introduction

Processing

Results

- SFE for the alloys $\text{Cr}_{14}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{26}$ and $\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$
- Processing route to produce single phase FCC $\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$ with grain size $\sim 20 \mu\text{m}$
- Critical twinning stress for the alloy $\text{Cr}_{14}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{26}$ and $\text{Cr}_{26}\text{Mn}_{20}\text{Fe}_{20}\text{Co}_{20}\text{Ni}_{14}$

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Norbert Lindner
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**Thanks for
your
attention**

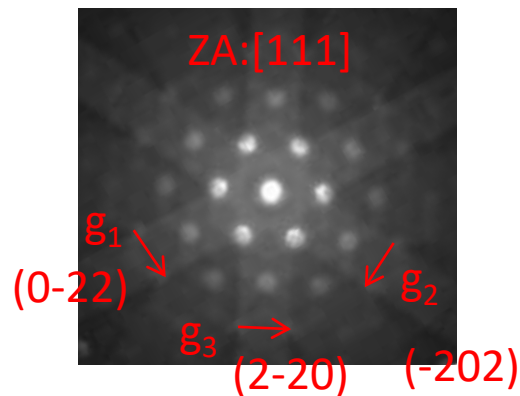
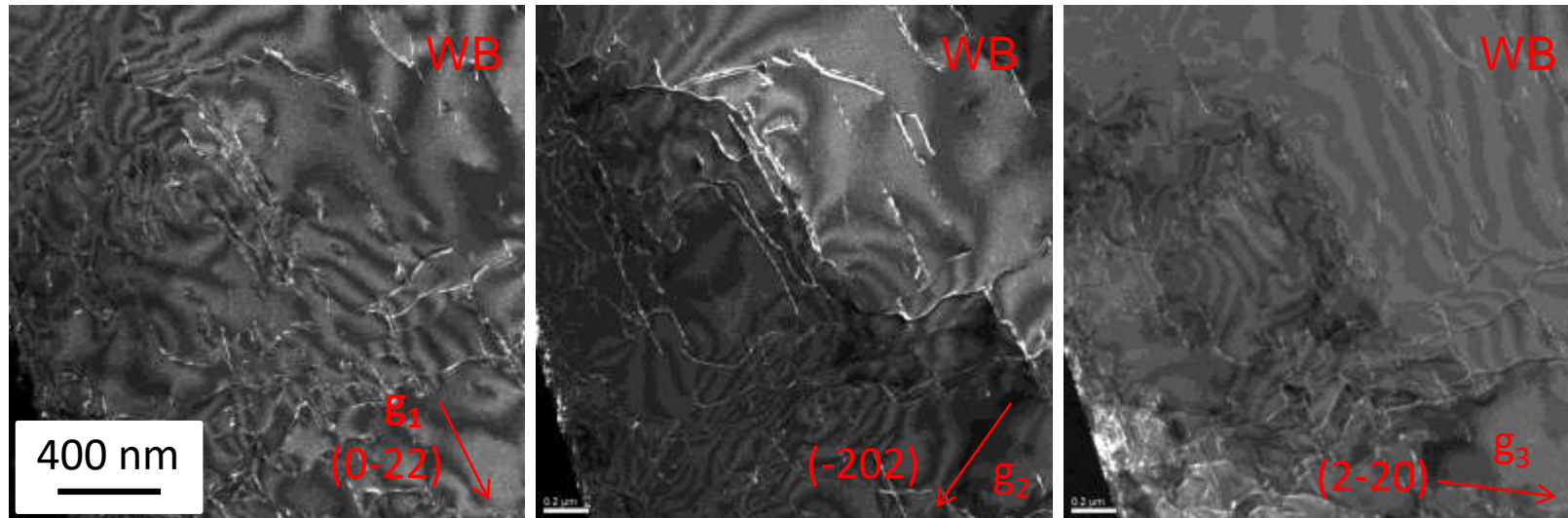
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Results – Work hardening rate

Stacking fault energy (SFE)

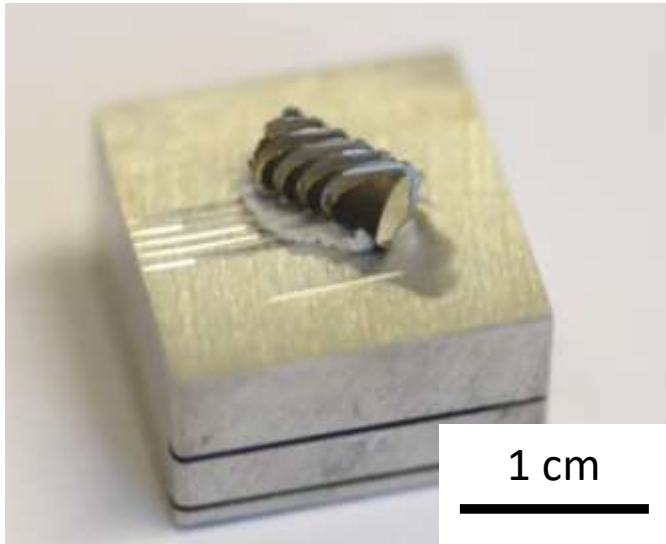


- $\text{Cr}_{14}\text{MnFeCoNi}_{26}$ at RT 4 % compressed
- Spacing could not be measured exactly

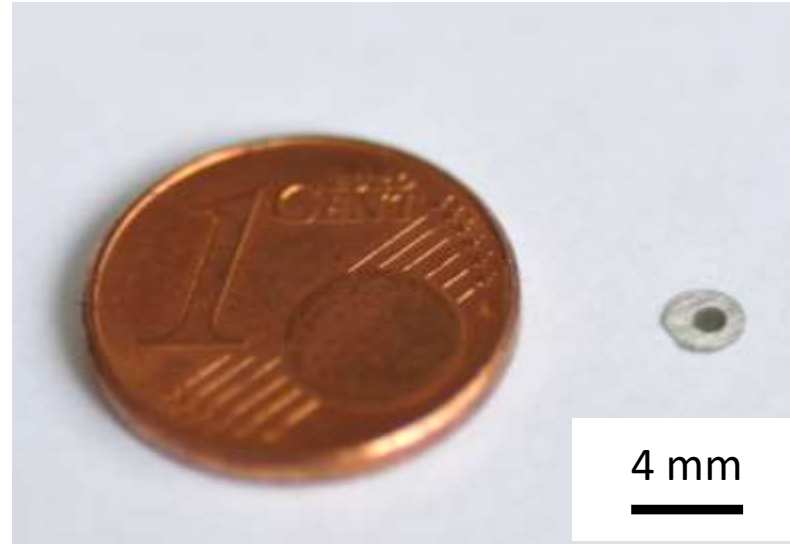
Stacking fault energy analysis

Twin jet electro polishing

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Compression sample cut in slices



TEM sample after the electro polishing

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