



Mechanical characterization of modified Compositionally Complex Alloy (CCA) $Al_{10}Co_{25}Cr_8Fe_{15}Ni_{36}Ti_6$ (in at.%) at elevated temperatures

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- Introduction:
 - Development of Al₁₀Co₂₅Cr₈Fe₁₅Ni₃₆Ti₆
- Characterization of base alloy
- Aims and goals of the project
- Microstructural optimization
- Alloy manufacturing
- Mechanical characterization
- Outlook





Starting point:

Equiatomic & multicomponent alloy system AlCoCrCuFeNi

- more than 6 (bcc) phases
- brittle



High Entropy Alloy (HEA)

Optimization steps:

- Elimination of segregation-element Cu
- Increase of face-centered cubic Ni
- Addition of Ti
- $\succ Al_{10}Co_{25}Cr_8Fe_{17}Ni_{36}Ti_6$
 - no base element
 - good mechanical properties



Compositionally Complex Alloy (CCA)



<u>Needles:</u> Al-rich phase (4% volume fraction) Particle length (γ'): ~ 450 nm Volume fraction (γ'): ~ 40% Secondary γ' in the range of some nanometers



Characterization of $Al_{10}Co_{25}Cr_8Fe_{15}Ni_{36}Ti_6$



Chemical analysis (SEM/TEM*-EDS)

in at.%	Original composition	Needles	γ/γ -structure*	
			γ-matrix	γ '-precipitates
Al	10	28	7	
Ni	36	33	30	45
Ti	6	7	3	8
Fe	15	10	21	9
Co	25	19	30	23
Cr	8	3	9	4

High Al-content in needle-phase, due to a decrease of Ni and especially Fe, Co and Cr Co-, Cr-, Fe-rich matrix Al-, Ti-, Ni-rich precipitates

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Aims and goals



- Optimization of γ/γ´-morphology (volume fraction & particle size)
 > Improvement of heat treatment
- Addition of trace elements (max. 1 at.%)





Base alloy: Optimization of heat treatment





Cubic shape of γ '-particles

Size and volume-fraction of γ -particles



Same kind of distribution of Al-rich needle phase



Addition of Hafnium



$Al_{9,5}Co_{25}Cr_8Fe_{15}Ni_{36}Ti_6Hf_{0,5}$ (in at.%)





- Eutectic formation at grain boundaries; T(hom) ≠ 1220°C
 - \succ T(hom) = 1140°C
- Spheric shape of Alrich needle phase
- Optimization of heat treatment







Addition of Molybdenum



$Al_9Co_{25}Cr_8Fe_{15}Ni_{36}Ti_6Mo_1$ (in at.%)



Nickel-based superalloys:

- Molybdenum enters matrix and precipitates
- Solid solution
 strengthening of matrix
- Reduction of misfit between γ and γ´
- Spheric shape of γ⁻particles
- Optimization of heat treatment





Alloy manufacturing: Directionally solidification



Induction casting



"Bridgman process"

Vacuum extraction	5·10 ⁻⁴ mbar
Casting atmosphere	Argon
Mould temperature	1400 °C
Initial weight	300 g
"Pull-down speed"	3 mm/min





Mechanical characterization





- Substance of examinations:
 - High temperature tensile tests (RT, 600°C, 700°C, 800°C, 900°C, 1000°C)
 - Creep experiments







- Al₁₀Co₂₅Cr₈Fe₁₅Ni₃₆Ti₆ as a promising material for applications at elevated temperatures (700 800°C)
- Microstructural changes due to the addition of molybdenum and hafnium
- Successful heat treatment optimization steps respective microstructural improvement
- DS-alloy manufacturing by induction casting & Bridgman process
- Outlook:
 - Creep and high-temperature tensile testing
 - Polycrystalin samples
 - > Influence of sample-orientation $(0^\circ, 45^\circ, 90^\circ)$
 - > Investigation of $Al_{10}Co_{25}Cr_8Fe_{15}Ni_{36}Ti_6$ + Zr, B, C, W, Y





Thank you for your attention!

